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... : ... : ... ,2016. 69

5321300-«  
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... . ... ( )



1497-73.

$l-$

$l_0-$

$d_0-$

$d_k-$

$a-$

$b-$

$F_0-$

$F_k-$

$l_k-$

$P-$

P

P

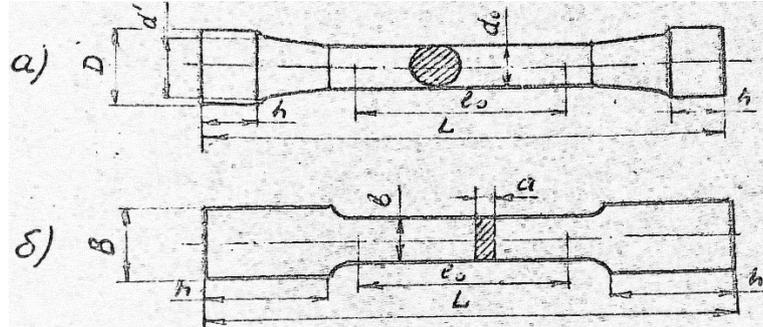
3

4

0,5

$$l_0 = 5,65 F_0 \quad , \quad l_0 = 11,3 F_0 \quad , \quad l_0 = 11,3 F_0 -$$

$$d_0 = 10 \quad (1.1)$$



.1.

$$= \frac{P_{max}}{F_0} \quad (1.1)$$

$P_{max}$

$$\delta = \frac{l_k - l_0}{l_0} \cdot 100\% \quad (1.2)$$

$l_k$

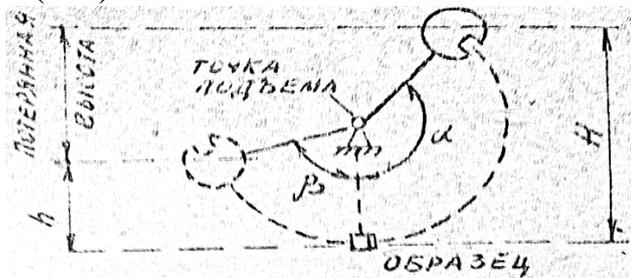
$d_k$

$$\psi = \frac{F_0 - F_k}{F_0} \cdot 100\% \quad (1.3)$$

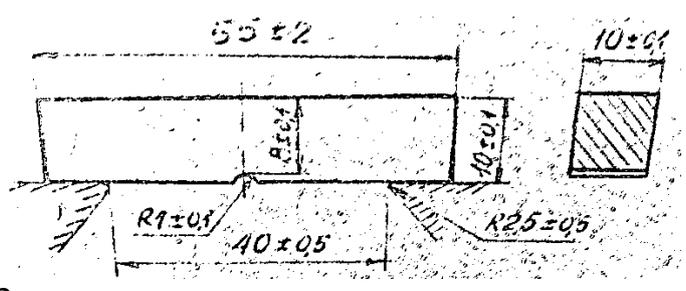
$$a_H = \frac{A_H}{F} \quad (1.4)$$

$$A_H = P \cdot l (\cos\beta - \cos\alpha) \quad (1.5)$$

$$\alpha_H = \frac{Pl(\cos\beta - \cos\alpha)}{F} \quad (1.6)$$



.2.



.3.

1.3.

1.4.

1.

2.

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6.

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( .3)

4.

5.

1.5.

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1.6.

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1

								$P_m$				
									$\sigma_B$	$\delta$ %	%	
		$d_0$	$l_0$	$F_0$	$l_K$	$d_K$	$F_K$					



( )

*F*:

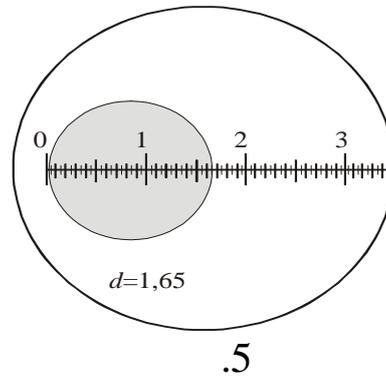
·  
:

$$\begin{aligned}
 &= 30D^2, \\
 P &= 10D^2, \\
 &= 2,5D^2.
 \end{aligned}$$

$$0,2D < d < 0,6D. \quad (2.3)$$

.5

0,05 ( )



(2.2).

( ,  $\sigma$  )

$$\sigma = \cdot HB [ ], \quad (2.4)$$

ó

( 0,160,7 % C) = 3,3í 3,4  
 ( 0,861,3 % C) = 3,5í 3,6  
 = 4,0  
 = 4,8

) , ( ,

:

$$\sigma = \frac{10 \cdot (HB - 40)}{6} [ \quad ].(2.5)$$

2.3.

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2.4.

- 1.
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- 7.

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2.5.

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2.6.

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3.1.  
ó

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3.2.

:

*Fe-C-*

).

(

Fe-C

(Fe-C),

*Fe-Fe<sub>3</sub>C* ( - ).

(Fe ).

911<sup>0</sup>

(Fe ).

932<sup>0</sup>C

(Fe ).

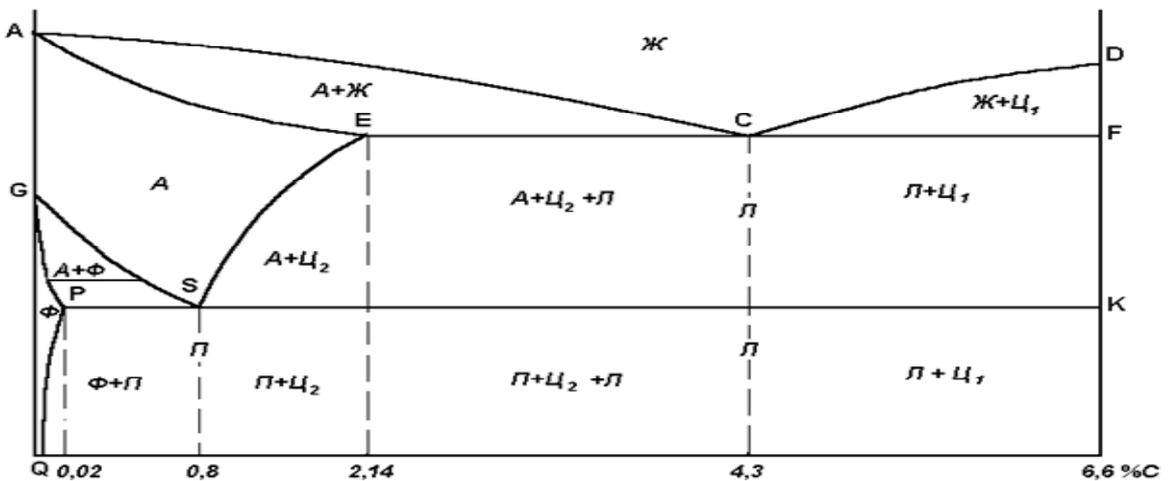
:

- 1) ( ) ó Fe .  
727° ó 0,025 % , 20° ó 0,006 % .
- 2) ( ) ó Fe .  
1147° ó 2,14% , 727° ó 0,83% .
- 3) ( ) ó Fe<sub>3</sub>C .  
6,67% .

δKö ( . 1) ó  
( + ) .

$$Q_{\phi} = \frac{HB}{AB} \cdot 100\% , \quad (3.1)$$

$$Q_a = \frac{AK}{AB} \cdot 100\% \quad (3.2)$$



.б.

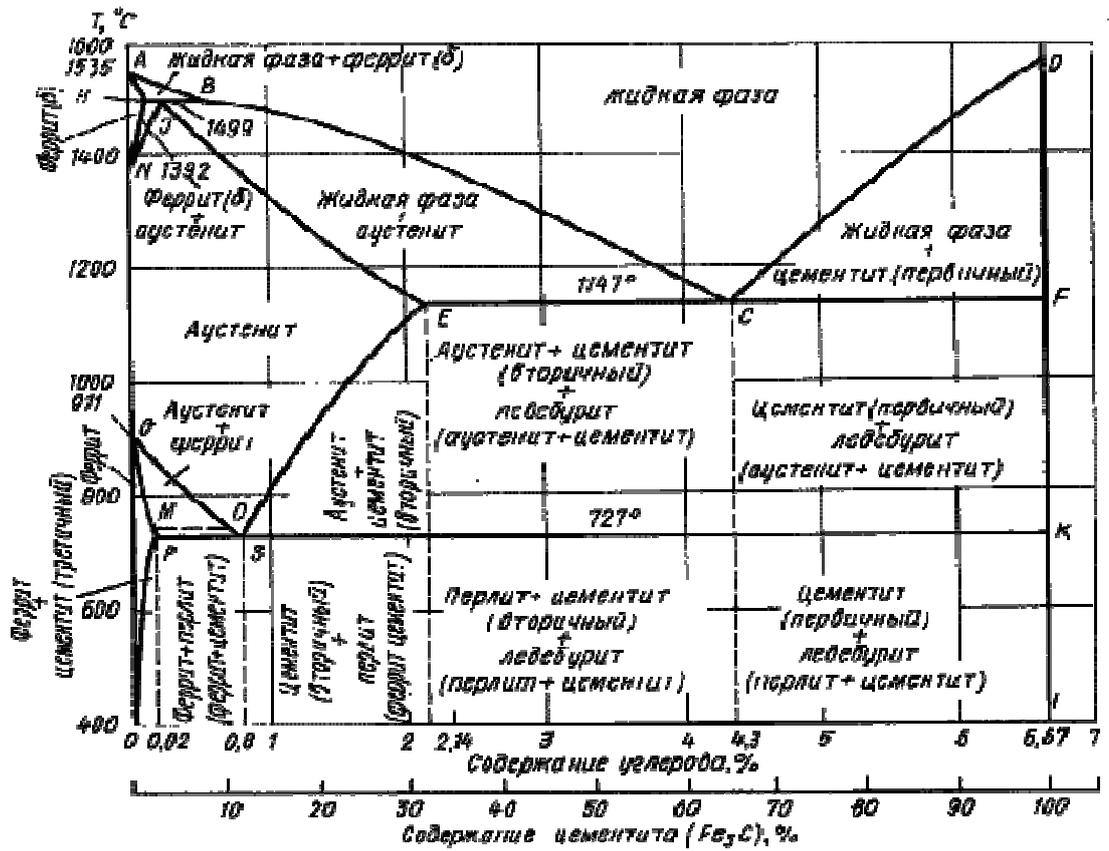
Fe-Fe<sub>3</sub>C

(100%).

( , )

4,3 %

0,8%



.7.

Fe-Fe<sub>3</sub>C

Fe-C

(.7)  
Fe-Fe<sub>3</sub>C

Fe-Fe<sub>3</sub>C

δAö.

- 1) (210) ó (Fe<sub>3</sub>C). 210 Fe<sub>3</sub>C, 210
- 2) <sup>1</sup>(727) ó ( )
- 3) <sup>2</sup>(768) ó 768
- 4) <sup>3</sup> ó GS,
- 5) - SE, ( )
- 6) 1147 ó ( )
- 7) ó
- 8) AECF- ( )

0,5% .  
 0,5%.  
 ( 1, .6).  
 (1,2,3,4) .  
 ó  
 =0,5%( .6).  
 ( , 4-4),

**3.3.**

Fe-C,  
 Fe-C,

**3.4.**

1.

Fe ó C (Fe ó Fe<sub>3</sub>C).

2. ( ).
3. ( ).
4. ( %).
- 3.5.  $t_1$ ,  $t_2$  ( ).
- ; Fe ó
- Fe<sub>3</sub>C ;
- ;
- .
- 3.6. : Fe ó C;
- Fe ó
- C;
- Fe ó C;
- %-
- 
- Fe ó C (Fe ó Fe<sub>3</sub>C)

1	2	1	2
1. $t_1=0.3\%$	$t_2=4.5\%$	$t_1=800^{\circ}\text{C}$	$t_2=1000^{\circ}\text{C}$
2. $t_1=0.9\%$	$t_2=3.5\%$	$t_1=900^{\circ}\text{C}$	$t_2=1200^{\circ}\text{C}$
3. $t_1=0.5\%$	$t_2=5\%$	$t_1=1450^{\circ}\text{C}$	$t_2=700^{\circ}\text{C}$
4. $t_1=0.4\%$	$t_2=3.0\%$	$t_1=1000^{\circ}\text{C}$	$t_2=950^{\circ}\text{C}$
5. $t_1=1.8\%$	$t_2=6.0\%$	$t_1=1300^{\circ}\text{C}$	$t_2=1850^{\circ}\text{C}$
6. $t_1=0.7\%$	$t_2=4.0\%$	$t_1=900^{\circ}\text{C}$	$t_2=600^{\circ}\text{C}$
7. $t_1=1.4\%$	$t_2=3.0\%$	$t_1=800^{\circ}\text{C}$	$t_2=1050^{\circ}\text{C}$
8. $t_1=0.6\%$	$t_2=4.8\%$	$t_1=1450^{\circ}\text{C}$	$t_2=1200^{\circ}\text{C}$
9. $t_1=1.2\%$	$t_2=5.5\%$	$t_1=750^{\circ}\text{C}$	$t_2=900^{\circ}\text{C}$

10.	$\alpha_1=0.45\%$	$\alpha_2=2.8\%$	$t_1=1000^{\circ}\text{C}$	$t_2=500^{\circ}\text{C}$
11.	$\alpha_1=0.2\%$	$\alpha_2=2.2\%$	$t_1=1200^{\circ}\text{C}$	$t_2=600^{\circ}\text{C}$
12.	$\alpha_1=0.5\%$	$\alpha_2=2.7\%$	$t_1=750^{\circ}\text{C}$	$t_2=800^{\circ}\text{C}$
13.	$\alpha_1=1.1\%$	$\alpha_2=3.2\%$	$t_1=1000^{\circ}\text{C}$	$t_2=1200^{\circ}\text{C}$
14.	$\alpha_1=0.3\%$	$\alpha_2=3.6\%$	$t_1=600^{\circ}\text{C}$	$t_2=1500^{\circ}\text{C}$
15.	$\alpha_1=1.6\%$	$\alpha_2=4.6\%$	$t_1=1400^{\circ}\text{C}$	$t_2=850^{\circ}\text{C}$
16.	$\alpha_1=1.9\%$	$\alpha_2=5.2\%$	$t_1=400^{\circ}\text{C}$	$t_2=1250^{\circ}\text{C}$
17.	$\alpha_1=0.55\%$	$\alpha_2=6.3\%$	$t_1=750^{\circ}\text{C}$	$t_2=1100^{\circ}\text{C}$
18.	$\alpha_1=0.7\%$	$\alpha_2=3.7\%$	$t_1=1450^{\circ}\text{C}$	$t_2=850^{\circ}\text{C}$
19.	$\alpha_1=0.9\%$	$\alpha_2=3.3\%$	$t_1=1100^{\circ}\text{C}$	$t_2=700^{\circ}\text{C}$
20.	$\alpha_1=0.4\%$	$\alpha_2=3.9\%$	$t_1=800^{\circ}\text{C}$	$t_2=400^{\circ}\text{C}$
21.	$\alpha_1=1.2\%$	$\alpha_2=4.2\%$	$t_1=700^{\circ}\text{C}$	$t_2=900^{\circ}\text{C}$
22.	$\alpha_1=1.4\%$	$\alpha_2=5.4\%$	$t_1=1350^{\circ}\text{C}$	$t_2=1300^{\circ}\text{C}$

#### 4

( )

4.1. :

1.

- ;

2.

, ( %),

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3.

, . ,

4.2.

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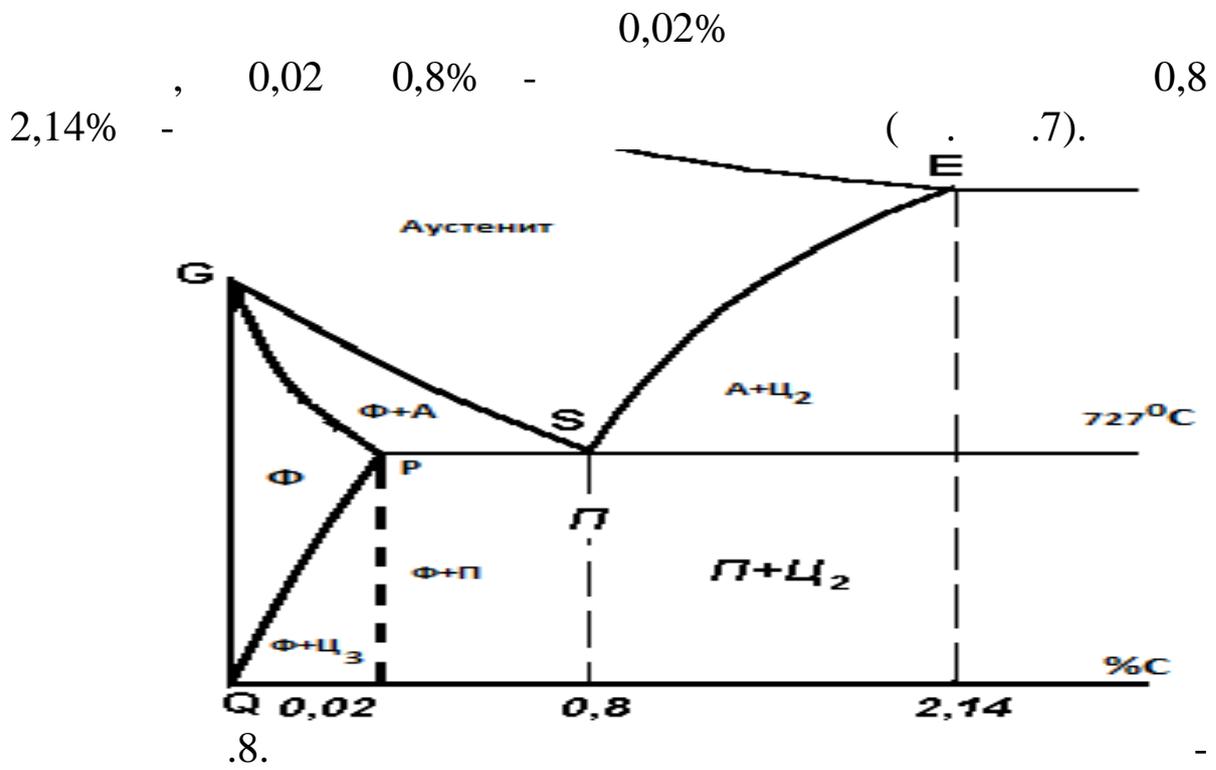
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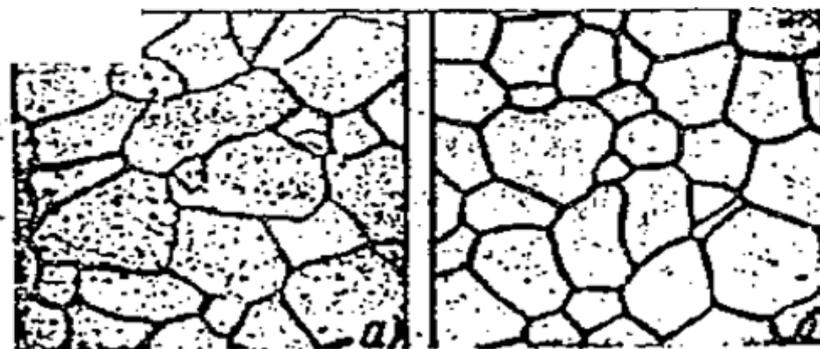
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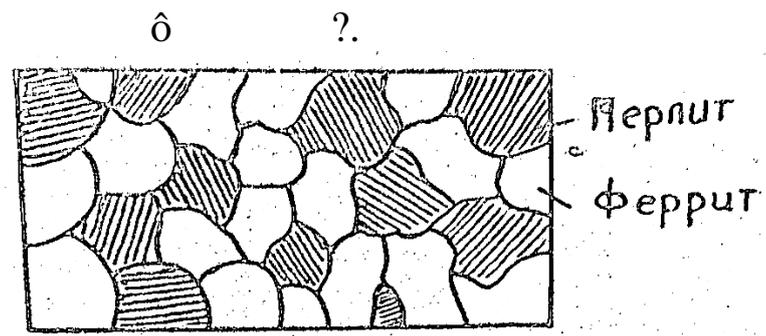


PS ( .8). ( ) ( .  
 727 °  
 - 0,006% .  
 0,006%  
 , . .  
 ( .9)



9. ; ) :

( 0,8% )  
 (0,8% )  
 9.



10.  
 ô ô  
 0,8% , . . . 0,8% .

$$C = \frac{F_n \cdot 0.8}{100} \% \quad (4.1)$$

$F_n$  ô , % .

, 70% ô , , 30%

$$C = \frac{70 \cdot 0.8}{100} = 0.56\% \quad (4.2)$$

55.

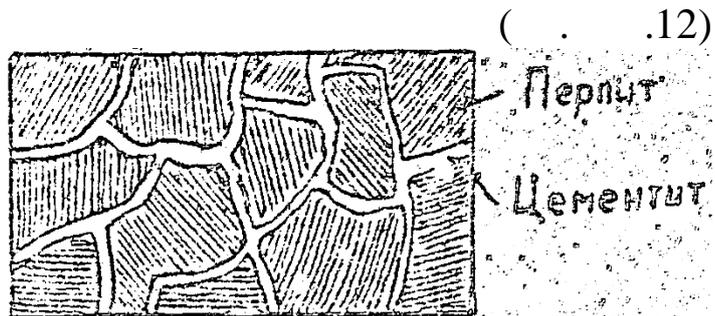


.11.

0,8 2,14%

$r_1$  ( PSK) ( . .8.) ( SE)

$r_1$



.12

$$C = \frac{F_{\pi} \% \cdot 0,8 + F_{\text{u}} - 6,67\%}{100} \quad (4.3)$$

4.3.  $F_{\pi}^-$  , % ( )  
 $F_{\text{u}}^-$  , % ( )  
 , , , ,  
 :

4.4. 1. 2-3 ( 3-4 ).  
 2.

3.

4. ( )

5.

6. , ,

7. ( )

4.5. :

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4.6. :

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 — ;  
 — 0.8%;  
 — ;  
 — .

4

					$\sigma_{\text{E}}$	$\delta_{\text{E}}$	$\alpha_{\text{E}}$		

5

**5.1.** :  
 ( ) , , .  
 , , .

**5.2.** : ,  
 ) ( ,  
 50 2000 .

2,14 6,67% . ,  
 , .

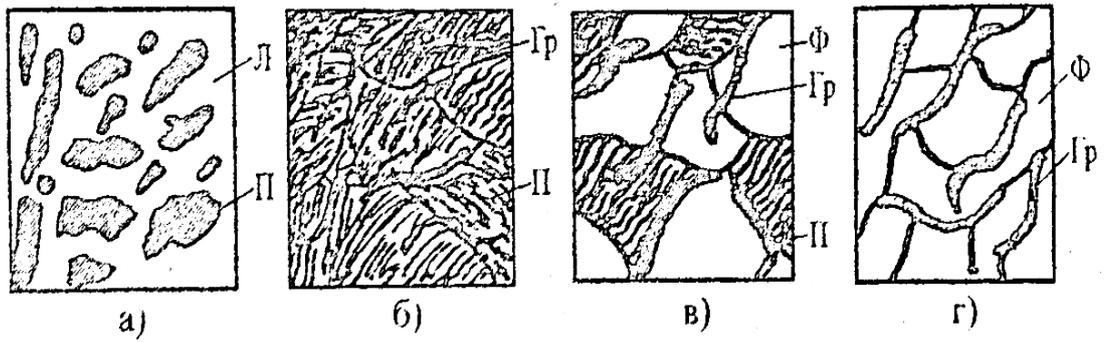
(Fe<sub>3</sub>C). : ( 2,14

4,3% ) + , (4,3%)  
 + , (.13, ).

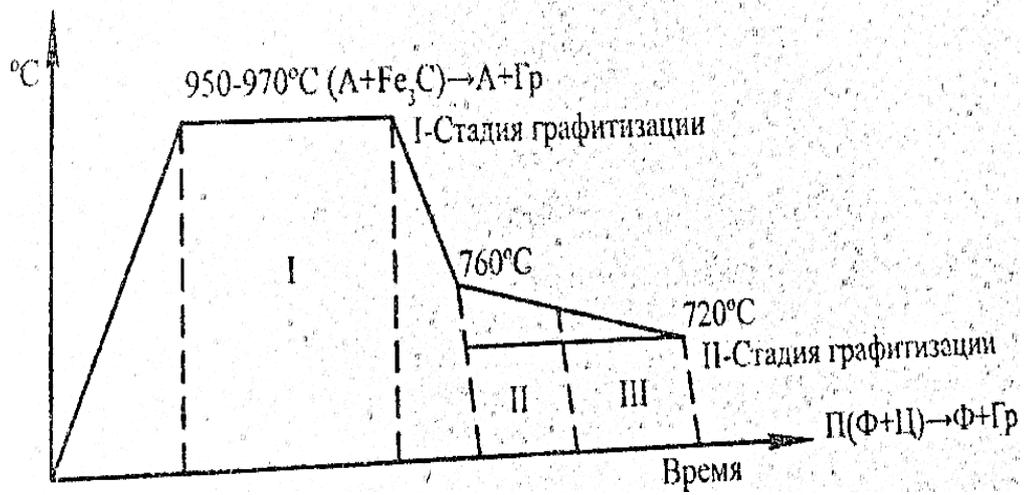
1) + ,  
 .(13, ).  
 2) + + ó -  
 ( .13, ).  
 3) + ó  
 .1, .  
 : 10, 15, 20, 25, 30,  
 40,  
 ( / <sup>2</sup>).

.  
 : , -  
 3-  
 .14 .  
 1- , +  
 .(14 ).  
 2- - ,  
 + + .(14 ).  
 3- , =  
 .2 .  
 : 30-6, 33-8, 50-4, 56-4,  
 60-3,  
 / <sup>2</sup>, ó  
 %.

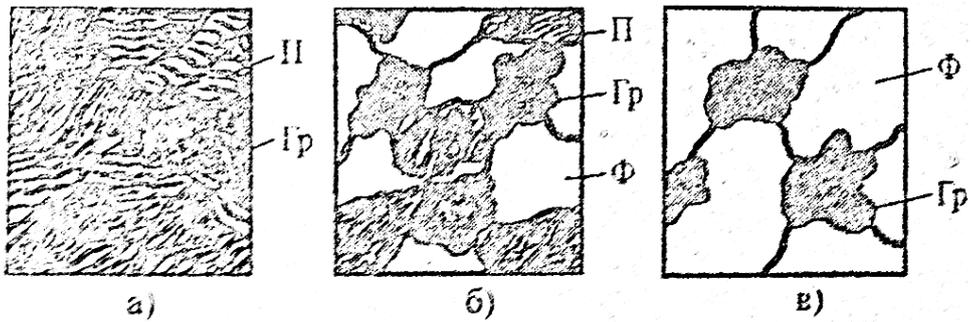
( ) .  
 , + , (15, ), ó  
 , + + .(15, ),  
 + .14 , .  
 : 42-12, 45-5, 50-  
 2, 60-2, 70-3, 80-3, 100-4 120-4,  
 , ó



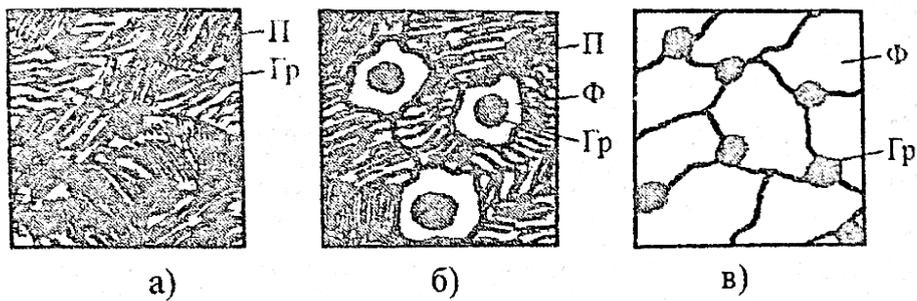
.13.



.14.



.15.



.16.

5.3. , , ,  
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 ( , , , )  
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5.4. :  
 3-4 .

1. :
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8. , ,
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10. .

5.5. :  
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5.6.

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5

1	2	3	4	5	5			
					$\frac{1}{2}$	$\frac{1}{2}$	$\frac{a_H}{\text{КГС} \cdot \text{М}} \text{ см}^2$	%
1	2	3	4	5	6	7	8	9
2								
3								
4								

6

6.1.

:  
 , ,  
 ,

6.2.

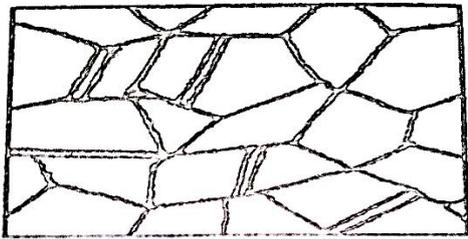
1.

:  
 . - ( , )

:

	00	0	1	2	3	4
%	9.99	9.95	9.9	9.7	9.5	9.0

( .17.)



.17.

$$\sigma_B = 240 \text{ МПа} = 45\%$$

$$\sigma_{0.2} = 50 \text{ МПа}$$

45%.

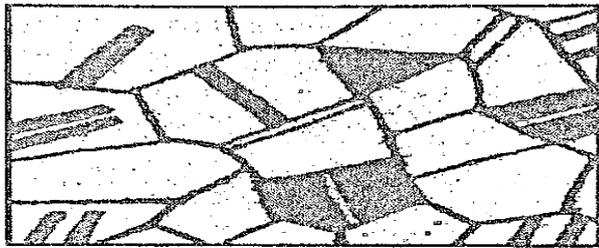
60%

60

1) - ,

39%,

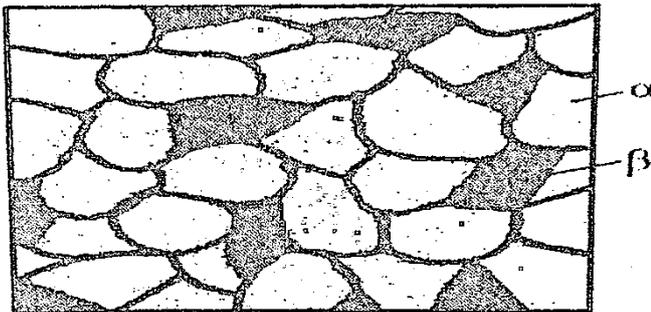
( .18.)



.18.

( ). : 60, 63, 68, 70, 80, 85, 90, 96.

2) + 39-45% (.19.)

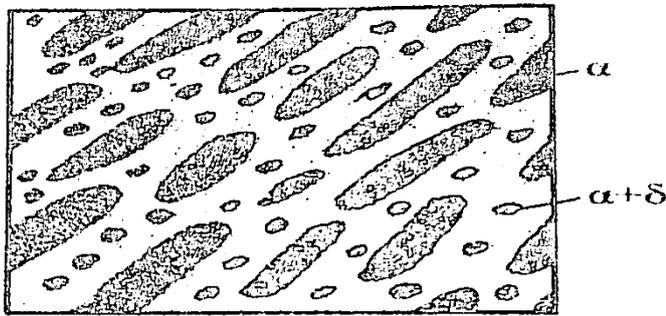


.19.

+ , , 59.

57 60% 59-1 : 0.8-1.5%

$\text{Cu}_{31}\text{Sn}_8$ .



.20.

( .21.)

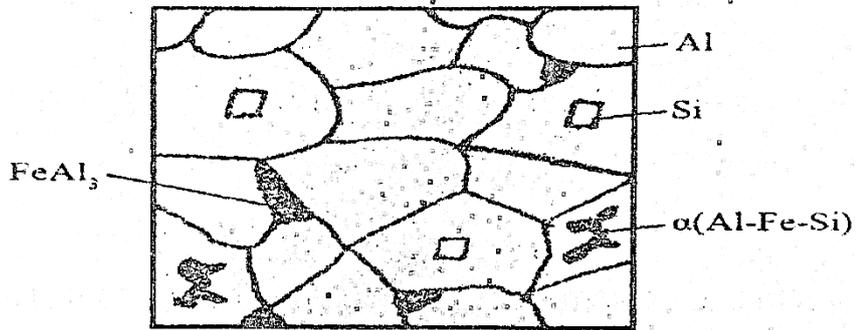


.21

2.

FeAl<sub>3</sub>

(.22.)



.22.

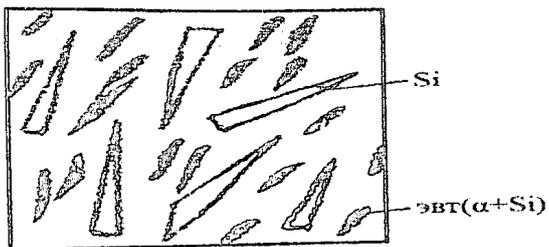
(6-14%).

2.

(+Si)

( )

(.23.)

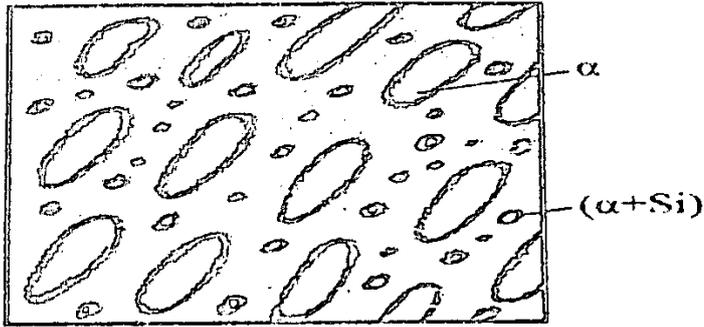


.23.

(0.01-0.1%).

( +Si)

( .24.)



.24.

(3.8-4.8%)

(0.4-1.8%),  
0.3-0.9%.

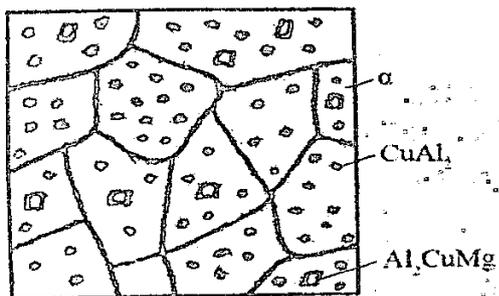
16.

$CuAl_2$  (

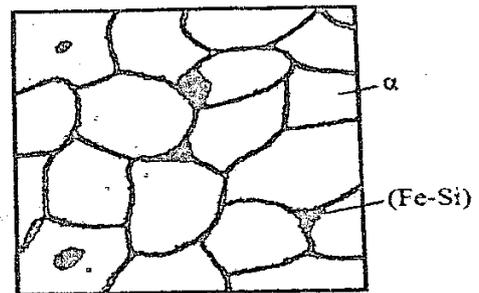
$Al_2CuMg$  (

).

( .25.)



a)



b)

.25.

16: - ; -

3.

81-84%

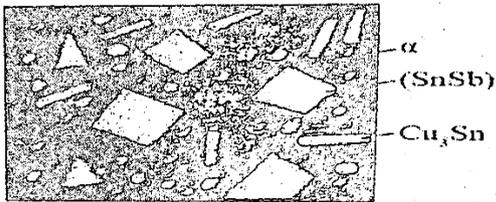
, 10-12%

5-6%

83

( ),  
SnSb

Cu<sub>3</sub>Sn ( .26.)



.26.

83.

( =60-120 , 13-35),  
(220-320<sup>0</sup> ),  
10-20 100<sup>0</sup> ,

6.3.

-8, -21

( -3, -7, )

6.4.

:

1. .
2. - .
3. + .
4. , .
5. , .
6. .
7. .
8. .
9. .
10. .

1. :  
2 .  
35x35 , 35 .  
(2) .  
( ) ,  
(3) .  
(4) .  
(5) .  
(6,7,8,9) .  
(10) 6 .

- 6.5.** :  
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- ;  
- .
- 6.6.** :  
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6

1	2	3	4	5 , %					10
					6 ,	7 $\sigma_{\text{в}}$	8 $\delta$ , %	9 $\psi$ , %	
1	2	3	4	5	6	7	8	9	10
2									

7

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7.1.

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7.2.

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22







**7.3.**

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**7.4.**

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**7.5.**

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**7.6.**

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1	2	3	4	5	6	7
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3						
4						

8

8.1.

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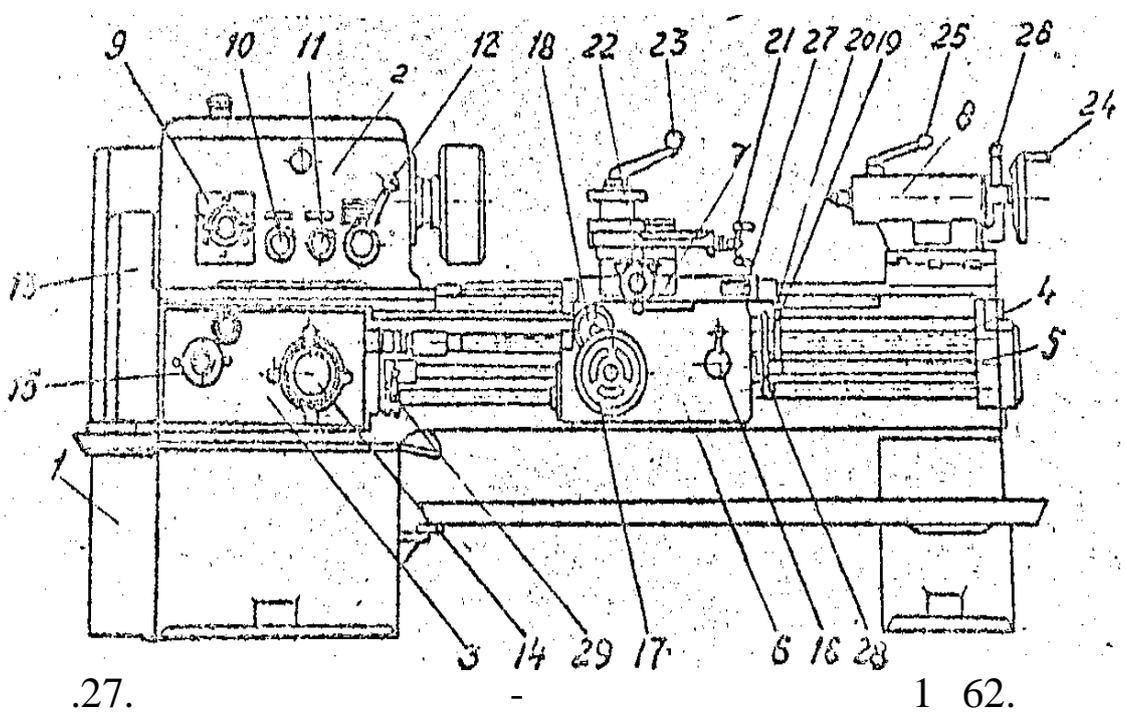
8.2.

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,	400
,	220
,	42
,	6
,	640, 930,
	1330
	24
, /	12,5-2000
, /	0,075-4,46
:	1-12
	2-24
	1
	0,51-48
í	8-32
,	10
, /	1450

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 ( 16 )

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(L>4 )

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 ( 9, 16, 1812 .), (9 , 5),  
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 - 5 10, 15 6, 14 8, 5 128, 8 6 ;  
 - 6, 8, 6 , 30 4,  
 15 10, 14 8, 15 6 .  
 6 ,  
 - 3, 3, 6, 8,  
 332.  
 80-85% ,  
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 ( -, -, - )  
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 ( L/ <4. )

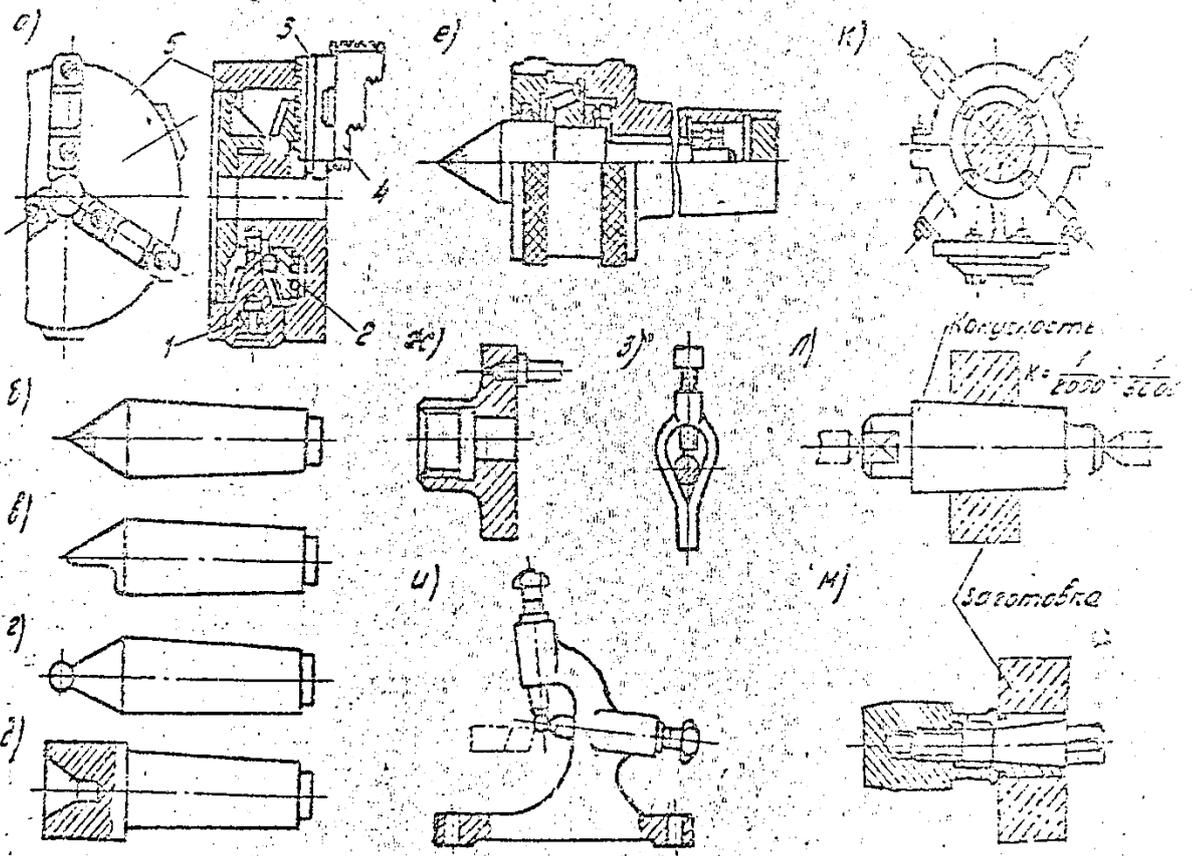
1, 2.  
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L/ =4í 10

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 ( )

: ( )-

. : ( )-  
 , ; ( )-  
 ; ; ( )-  
 . (L/ >10)  
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 ( ), ( ) , .  
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 ( , ), ( , ) ( , ),  
 ( ), ( ) ( ) .



.28.

29

( )  
( ).

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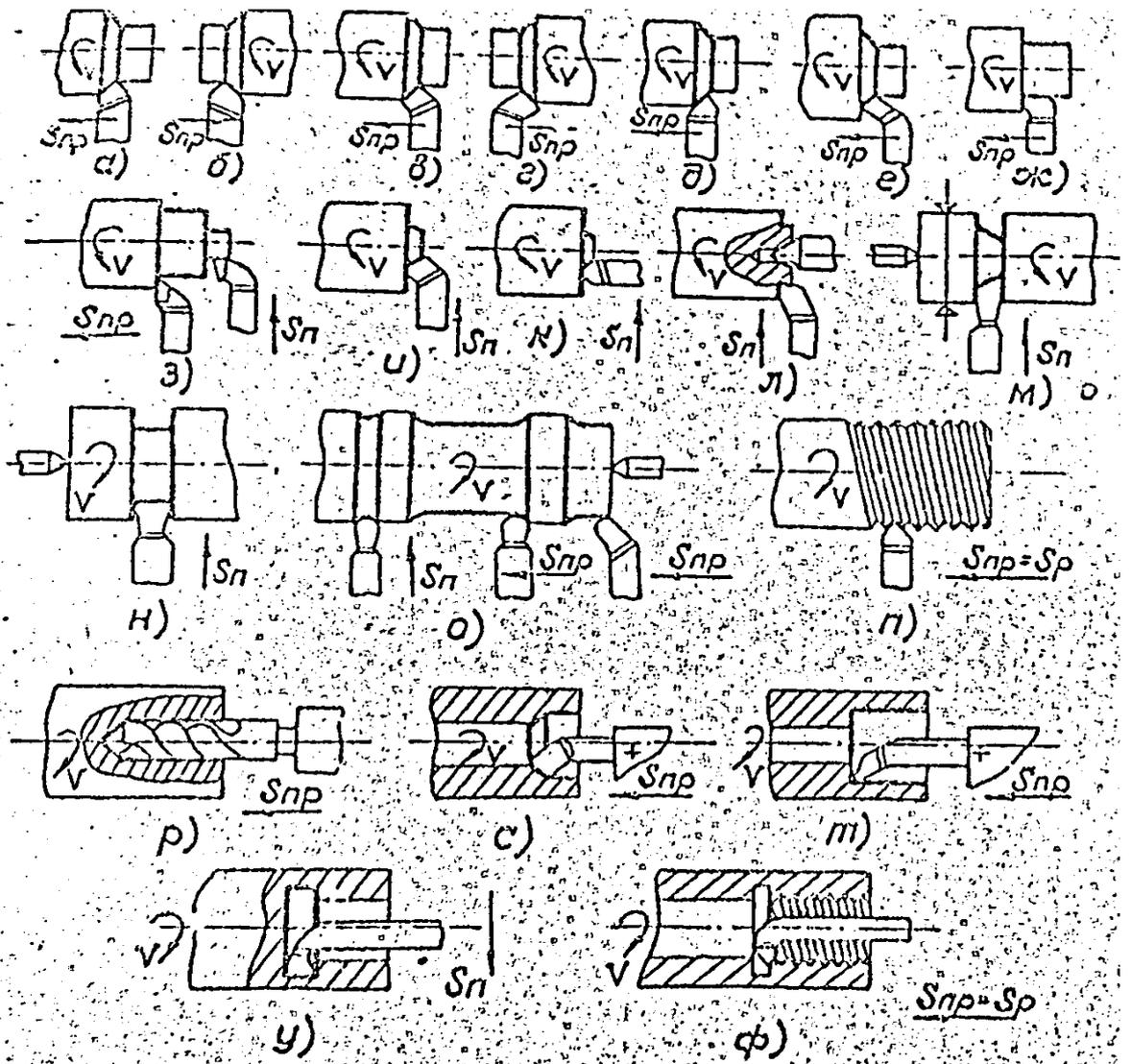
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$$tg\alpha = \frac{D-d}{2l} \quad (8.1)$$
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$$(2 = 8i \cdot 10^0) \quad (.30, )$$

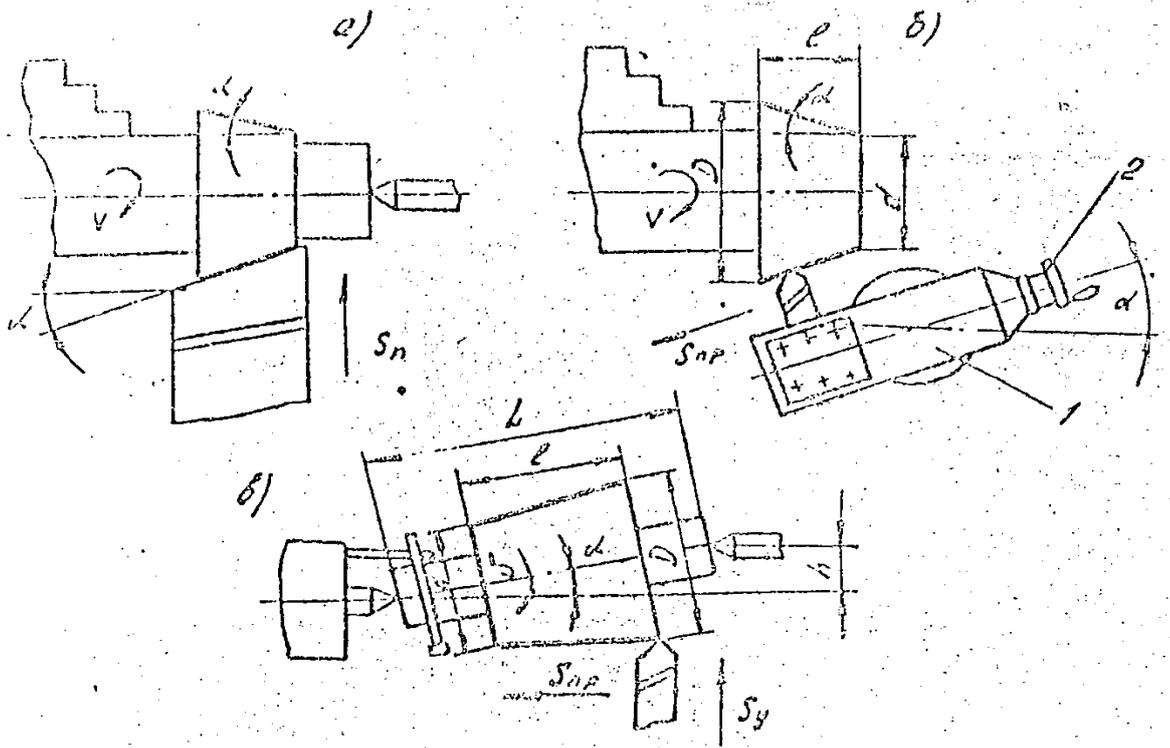
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$$h = \frac{L(D-d)}{2l} \quad (8.2)$$

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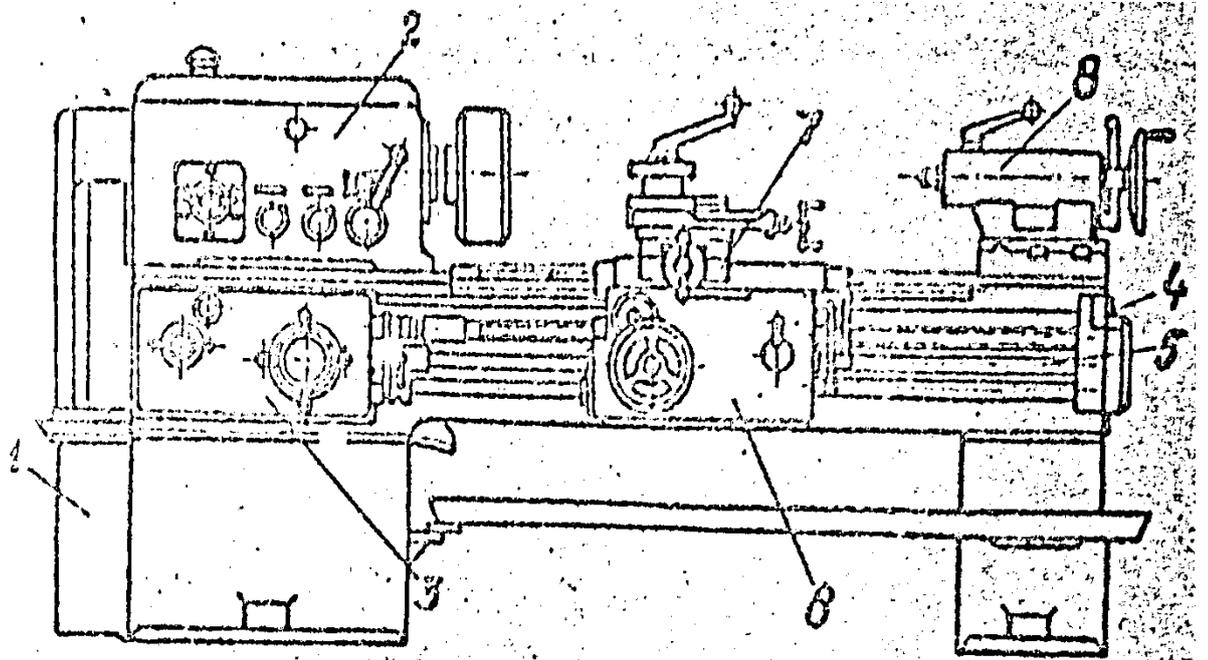
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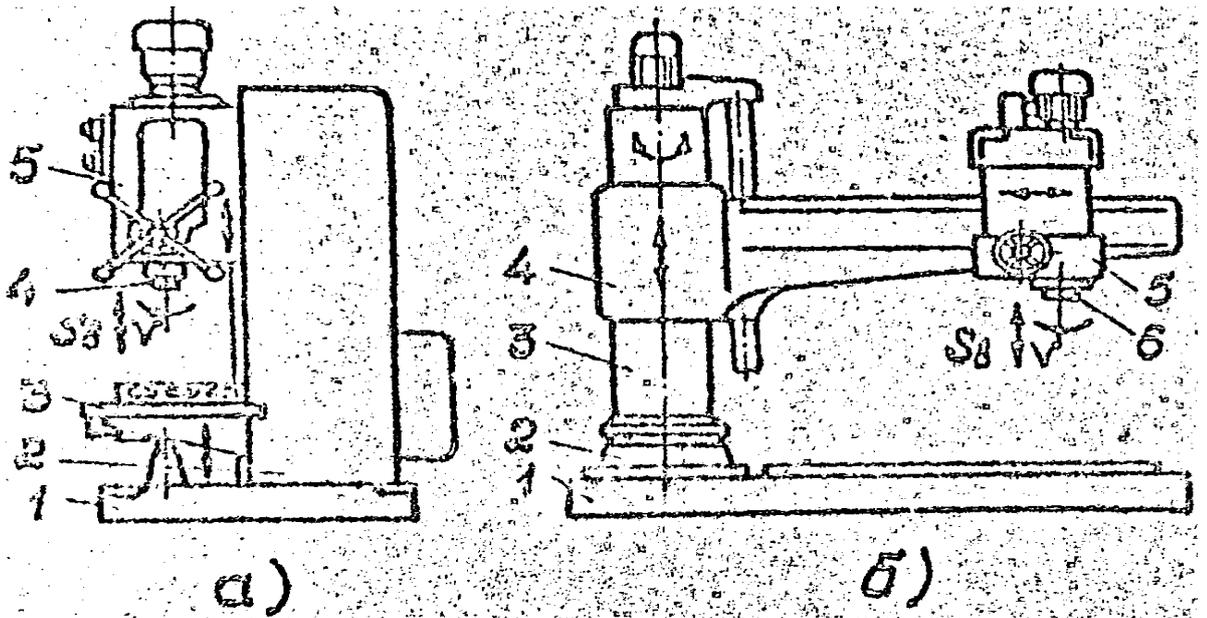
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9.2. :

$$(\sigma_B = 50 - 60 \frac{RT}{MM^2}) \quad (8.3)$$

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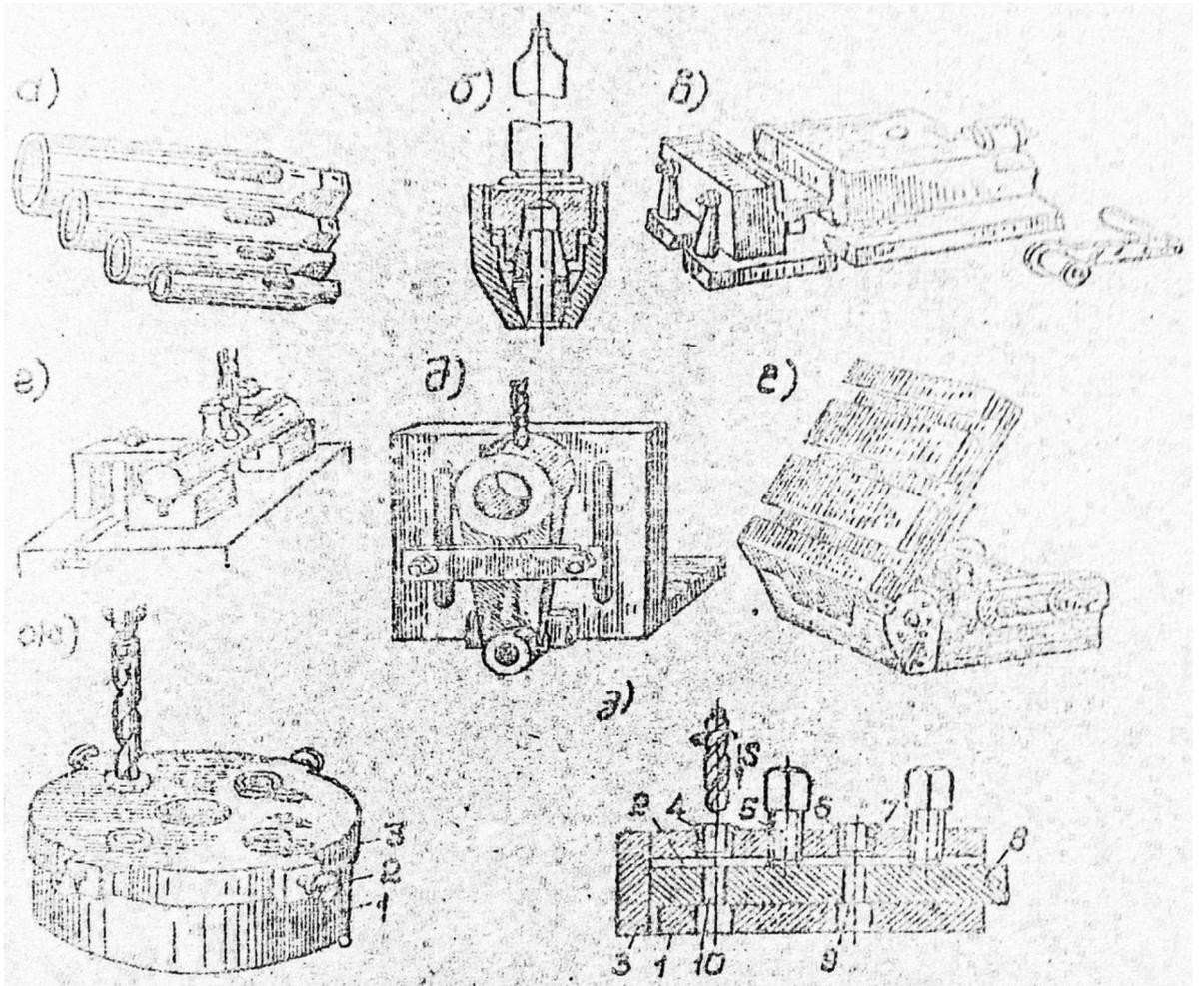
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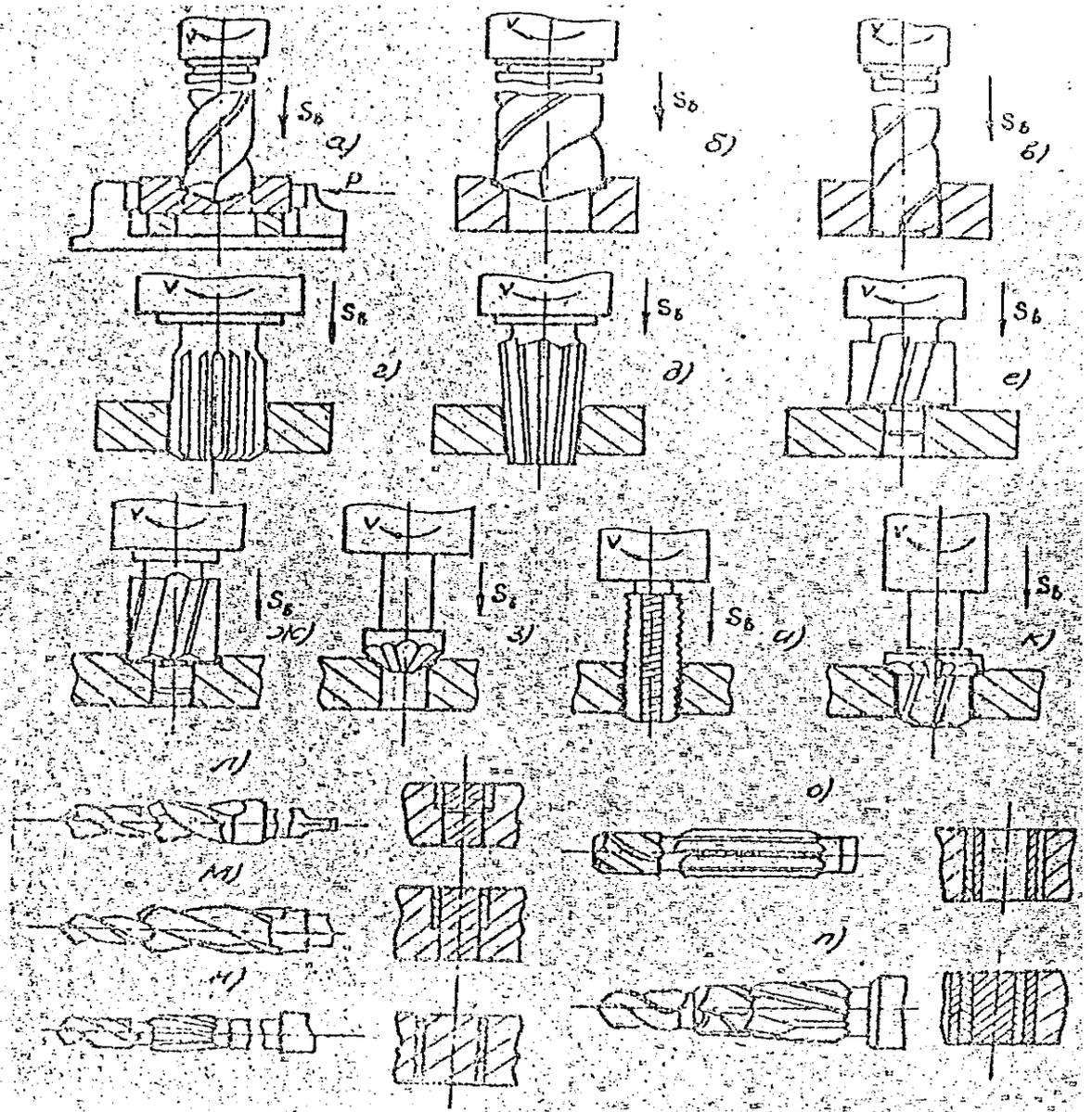
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